

Paper Feeding System Tutorial (AutoDesign)





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Edition Note

This document describes the release information of **RecurDyn V9R4**.

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Outline of Tutorial Sample E

Model	Description
Sample E	Paper Feeding System Design Problem: When a paper feeds through the roller system-2 and pass through the roller system-1. In a given time, the roller system-1 rotates reversely. Then, the paper runs the roller system-1 backward. The design goal is to minimize the slip between roller-system and paper while satisfying the nip force limitation.
	Key Point : Study the Expression for representing the slip phenomenon. Also, note the design modeling approach to use the guide position as design variable.



Paper Feeding System Design Problem

A paper feeds into the roller system-2 and runs through the roller system-1. When the end of paper passes at the event sensor position, the rotation direction of the roller system-1 is changed as reverse direction.

The design objective is to minimize the slip amount between the paper and the fixed roller in the roller system-1 while satisfying the nip forces of two roller systems for their limits. The design variables are the stiffness, damping and pre-load of nip springs and the rotation angle of the guide attached in the green colored dummy body.



Open files related in Sample-E					
Sample	<install dir=""> \Help\Tutorial\AutoDesign\PaperFeedingSystem\Examples\Sample_E.rdyn</install>				
Solution	<install dir=""> \Help\ Tutorial\AutoDesign\PaperFeedingSystem\Solutions\Sample_E.rdyn</install>				

Note: If you change the file path at discretion, it can be located in any folder that you specify.

Chapter

Loading the Model anv Viewing MTT2D Model

To load the base model and view the animation:

- RecurDyn
- 1. On your Desktop, double-click the **RecurDyn** tool.
- 2. RecurDyn starts and the **Start RecurDyn** dialog box appears.
- 3. Close **Start RecurDyn** dialog box. You will use an existing model.
- In the Quick Access toolbar, click the Open and select 'Sample_E.rdyn' from the same directory where this tutorial is located. (<Install Dir> \Help\Tutorial\AutoDesign\ PaperFeedingSystem\Examples)
 - 5. The paper feeding system appears in the modeling window. Click the center of model to switch model as MTT2D.
 - 6. Click the **Dynamic/Kinematic** button.

Start RecurDyn		×
New Model -		
Name	Model1	
Unit	MMKS(Millimeter/Kilogram/Newton/Second)	Setting
<u>G</u> ravity	-γ ▼	Setting
		<u>O</u> K
Open Model		Browse
Recent Mode	łs	Icons 🔻
Show 'Start	RecurDyn' Dialog when starting	



- **7.** Click the **Play** button.

The paper moves from left upper end to the right bottom end. The paper will hit the guides during it progresses.





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Defining the Design Variables

When you see the Parametric Value in the **SubEntity** menu, the following 10 parameters are listed. Among them, parameters 1~6 and 10 are the design variable.

The nip spring properties are linked to the parametric values as follows: Check Property of MovableRollerGroup2. Then, Nip Spring Property button is activated. Then, click the button. The below window will be shown. Then, define the Stiffness, Damping and **Pre Load** by using the parametric values.





Next, verify the dummy body as `**Body2**' and the Linear Guide to the dummy body.

Propertie	s of Body	2 [Current L	Jnit : N	/kg/ı	mm/s/deg]		
General	eneral Graphic Property Origin & Orientation Body						
Mater	Material Input Type				•		
Mater	ial Type		Steel		•		
Mass	4.6238668	3646668e-04					
bxx	1.1972029	6943871e-02	lxy	1.5	9294365074607e-02		
lyy	2.1728754	1181156e-02	lyz	0.			
Izz	3.3623698	5385539e-02	Izx	0.			
Volum	ie	58.90276224	79832		Show Property		
Cente	r Marker			СМ	I		
Inertia	a Marker	Crea	ate		IM		
Initial	Condition	on Initial Velocity					
Scope		(DK		Cancel Apply		

And check the rotational joint at the right end of **Body2**. This is used only to define the Motion. The parametric value of 'Guide_Control' is used to describe the **Motion** expression. When the analysis start, the body is rotated with the magnitude of 'Guide_Control'(deg.). Then, the guide will rotate with the same degree because it is attached to the **Body2**.

Properties of RevJoint34 [Current Unit : N/kg/mm/s/deg]	Motion
General Connector Joint	Motion
Type Revolute	Type Standard Motion
Initial Conditions Position (PV:R) Include Initial Conditions Strict Initial Conditions	Displacement (time) Expression Name Gude_Location Expression Guide_Control*DTOR*STEP(TIME,0,1,1,1)
Friction	
Force Display Inactivate 👻	
Scope OK Cancel Apply	OK Cancel Apply



Defining the Analysis Response

Although MTT2D provides the mean slips of each roller, they cannot be directly controlled in the Expression, which represents that they are not Analysis Response.

Thus, we make the slip amounts by using the **Expression**. The right **Expression** is the slip amount between the paper and the Fixed_roller body in 0.35 second.

Expression	
Name Ex3	
ABS((WZ(2, 1, 1)*Roller_13mm-SNSR(3))) *ST	EP(TIME, 0.35, 0, 0.351, 1)
Available	Argument List
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	ID Entity 1 FixedRollerBody1.Marker1 2 MotherBody.Marker1 3 SpeedSensor1
ОК	Cancel Apply

The Nip force can be represented by using the spring force.

Expression	
Name Nip_Force	
SPRING(1,1,1,2)*STEP(TIME,0.1,0,0.11,1)	
Available	Argument List
Eunction expressions F	ID Entity
$\oplus \pi$ Simulation constants \equiv	2 MotherBody.Marker3
telocity ↓	
Acceleration	
E F Specific force	
in fat System element	
	Add Delete
ОК	Cancel Apply

In **Analysis Response**, the analysis responses are defined as shown the figure below. AR1 is the maximum value of the nip spring force. AR2 is the absolute maximum and AR3 is the RMS of the expression, Ex3.

y 51 5	Response					
٧o	Name	Туре	Pr	Description	Treatment F	PI
1	AR1	Basic		Nip_Force_Max	Max ABS	I
2	AR2	Basic		Slip_Max in 0.35 sec	Max ABS	-
3	AR3	Basic		Slip_RMS in 0.35sec	RMS Value	

For the initial design, the expression Ex3 gives the following result, which may be highly nonlinear to the change of design variables.



Chapter

Running a Design Optimization Problem

The optimization problem is defined as:

Minimize the Maximum Peak of Slip and the RMS of Slip

subject to

Nip Force =< Limit

1. In the **Design Optimization** menu, the **Design Variable** tab shows the list of design variables.

De	Design Optimization								
D	Design Variable Performance Index Optimization Control Result Sheet Summary Sheet								
	DV	DP	Description	Current	LB	UB	Туре		Value
	1	DP1	Spring K1	1.e-03	1.e-04	1.e-02	Variable	-	0.
	2	DP2	Damping C1	1.e-04	5.e-05	5.e-04	Variable	-	0.
	3	DP3	Pre Load 1	5.e-02	1.e-02	0.1	Variable	-	0.
	4	DP4	Spring K2	1.e-03	1.e-04	1.e-02	Variable	-	0.
	5	DP5	Damping C2	1.e-04	5.e-05	5.e-04	Variable	-	0.
	6	DP6	Pre Load 2	5.e-02	1.e-02	0.1	Variable	-	0.
	7	DP7	Guide Angle	0.	0.	4.	Variable	-	0.

2. In the **Performance Index** tab, the above design formulation is defined as right. In this study, the limit of Nip force is used as 0.025(N/mm).

0	esign Op	otimiza	tion								
[Design Va	riable	Performan	ce Ir	odex Optimization Cor	ntrol Result Sheet	Summa	ary Sheet			
	PI	Use	AR		Description	Definition		Goal		Weight/Limit Value	
	1		AR1	-	Nip_Force_Max	Constraint	-	LE	-	2.5e-02	
	2		AR2	-	Slip_Max in 0.35 sec	Objective	-	MIN	-	1.	
	3		AR3	•	Slip_RMS in 0.35sec	Objective	-	MIN	-	1.	

3. In the **Optimization Control** tab, the convergence tolerances use the default values. Push **Execution** button for optimization analysis.

Design Optimization	
Design Variable Performance Index Optimization Control Result	Sheet Summary Sheet
DOE Meta Modeling Methods	Methods
Convergence Tolerance	
Objective Change Rate in Consecutive Iterations	5.e-02
Equality Constraints	1.e-03
Inequality Constraints	1.e-03
Maximum Iteration of SAO	30.
Convergence Relaxation Control	OFF 💌
Simulation Type	Dynamic/Kinematic 💌
Save Results Latin	Number of Trials 23
Analysis Setting	Execution
	OK Cancel Apply

4. Next, check the **Result Sheet** after the optimization is completed. **AutoDesign** is converged in 19 iterations. In the final design, the nip force is 0.0248 and the slip amounts such as the maximum peak and the RMS value are 4.44 and 0.955.

esign Variable	Performance Index	Optimization Control	Result Sheet	Summary Sheet		
Optimization H	listory of AR Values					
No	AR1	AR2		AR3	Violation	
16	2.47804013222426e-00	2 4.96117316049	9344	0.95944504673006	0.	
17	2.54464106694164e-00	2 5.39851344435	5613 0	0.976488521125728	0.	
18	2.47985136643638e-00	2 4.88918512378	3484 ().958711543664367	0.	
19	2.48434927148849e-00	2 4.83789095408	3923 0	0.955838311971229	0.	
	1 1					
🛩 🖻 🗠	🖾 🔯 👯 🔳 <	Þ 🕂 🎯 🕀 🖾	E 🚿 🕅	10		
35.00 30.00		<u>,</u>				
25.00	/ \					ject
15.00-					Maximum Viola	tion
10.00 -						
5.00-						
-5.00						
-5.00 -	2 3 4 5	6 7 8 9 10 SAO Iter	11 12 13 ation	14 15 16 17 1	8 19	

5. The Following figures compare the guide positions for the initial and the final designs. When the paper is reversely feed, the initial design hits the guide marked 'A' but the final design does not. Thus, the final design can reduce the slip.



Initial Design



Final Design



Comparison of Analysis Results

Now, we compare the analysis responses. First, compare the nip forces. The blue color line is the initial design and the red color line is the final design. This comparison shows that the final design satisfies the limitation.



Next, let's compare the slip amounts. The final design (red color line) is much less than the initial one (blue color line). From our empirical experience, the maximum slip peak, shown as sharply shaped mountain, is highly nonlinear. Thus, its approximation requires many sampling points. Although the shape of the nip forces seems to be sharp, it is however slightly nonlinear because their shapes have same trends according to the changes of design variables. The reason of non-smoothness of the maximum peak of slip amounts is due to the position of guide (DV7). Compare the guide position for the initial and the final design, which explains the non-smoothness.



Thanks for participating in this tutorial!